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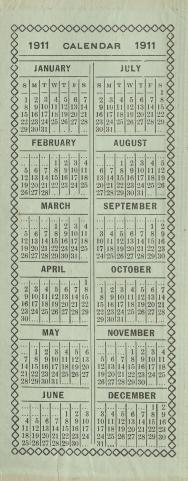
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It is our intention that this booklet shall be serviceable to you, as a convenient and durable memorandum, and serviceable to us as a reminder to our friends that we are persistently in the field for their business. Our part in every transaction is to give you honest value and perfect service.

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USEFUL INFORMATION.

WATER.

A Gallon of Water (U. S. Standard) contains 231 cubic inches and weighs 8½ pounds.

A Cubic Foot of Water contains 7½ gallons, or 1728 cubic inches, and weighs 62½ pounds.

A "Miner's Inch" is a measure for the flow of water, and is the amount discharged through an opening 1 inch square in a plank 2 inches in thickness, under a head of 6 inches to the upper edge of the opening; and this is equal to 11,625 U. S. gallons per minute.

The height of a column of fresh water, equal to a pressure of 1 pound per square inch, is 2.31 feet.

A column of water 1 foot high exerts a pressure of .433 pounds per square inch.

The capacity of a cylinder in gallons is equal to the length in inches multiplied by the area in inches, divided by 231 (the cubical contents of one U. S. gallon in inches).

The velocity in feet per minute, necessary to discharge a given volume of water in a given time, is found by multiplying the number of cubic feet of water by 144, and dividing the product by the area of the pipe in inches.

The area of a required pipe, the volume and velocity being given, is found by multiplying the number of cubic feet of water by 144, and dividing the product by the velocity in feet per minute. The area being found, the diameter is obtained by the table of areas.

Doubling the diameter of a pipe increases its capacity four times.

The friction of liquids in pipes increases as the square of the velocity. The horse-power necessary to elevate water to a given height is found by multiplying the weight of the water elevated per minute, in pounds, by the height in feet, and dividing the product by 33,000.

Pressure of Water Due to its Weight. The pressure of still water in pounds per square inch against the sides of any pipe, channel or vessel of any shape whatever is due solely to the "head." or height of the level surface of the water above the point at which the pressure is considered, and is equal to .433021b. per square inch for every foot of head, or 62,3551bs. per square foot for every foot of head (at 62° F.)

The pressure per square inch is equal in all directions, downwards, upwards, or sideways, and is independent of the shape or size of the containing vessel.

The pressure against a vertical surface, as a retaining-wall, at any point is in direct ratio to the head above that point, increasing from 0 at the level surface to a maximum at the bottom. The total pressure against a vertical strip of a unit's breadth increases as the area of a rightangled triangle whose perpendicular represents the height of the strip and whose base represents the pressure on a unit of surface at the bottom; that is, it increases as the square of the depth. The sum of all the horizontal pressures is represented by the area of the triangle, and the resultant of this sum is equal to this sum exerted at a point one-third of the height from the bottom. ("he center of gravity of the area of a triangle is one-third of its height.)

The horizontal pressure is the same if the surface is inclined instead of vertical.

(For an elaboration of these principles see Trautwine's Pocket-Book, or the chapter on Hydrostatics in any work of Physics. For dams, retaining-walls, etc., see Trautwine.)

The amount of pressure on the interior of walls of a pipe has no appreciable effect upon the amount of flow.

Buoyancy. When a body is immersed in a liquid, whether it float or sink, it is buoyed up by a force equal to the weight of the bulk of the liquid displaced by the body. The weight of a floating body is equal to the weight of the bulk of the liquid that it displaces. The upward pressure or buoyancy of the liquid may be regarded as exerted at the center of gravity of the displaced water, which is called the center of pressure or of buoyancy. A vertical line drawn through it is called the axis of buoyancy or of flotation. In a floating body at rest a line joining the center of gravity and the center of buoyancy is vertical, and is called the axis of equilibrium. When an external force causes the axis of equilibrium to lean, if a vertical line be drawn upward from the center of buoyancy to this axis, the point where it cuts the axis is called the metacentre. If the metacentre is above the centre of gravity the distance between them is called the metacentric height, and the body is then said to be in stable equilibrium, tending to return to its original position when the external force is removed.

Boiling-Point. Water boils at 212° F. $(100^{\circ}$ C.) at mean atmospheric pressure at the sea-level, 14.7 lbs, per square inch. The temperature at which water boils at any given pressure is the same as the temperature of saturated steam at the same pressure.

The Boiling-Point of Water may be Raised. When water is entirely freed of air, which may be accomplished by freezing or boiling, the cohesion of its atoms is greatly increased, so that its temperature may be raised at 50° above the ordinary boiling-point before ebullition takes place. It was found by Faraday that when such air-freed water did boil, the rupture of the liquid was like an explosion. When water is surrounded by a film of oil, its boiling temperature may be raised considerably above its normal standard. This has been applied as a theoretical explanation in the instance of boiler explosions.

The freezing-point also may be lowered, if the water is perfectly quiet, to 10° C, or 18° Fahrenheit below the normal freezingpoint. (Hamilton Smith, Jr., on Hydraulics, p. 13.) The density of water at 14° F., is .99814, its density at 39.1° F. being I, and at 32° F., 99987.

Freezing-Point. Water freezes at 32° F., at the ordinary atmospheric pressure, and ice melts at the same temperature. In the melting of 1 pound of ice into water at 32° F., about 142 heat units are absorbed, or become latent; and in freezing 1 pound of water into ice a like quantity of heat is given out to the surrounding medium.

Sea-Water freezes at 27° F. The ice is fresh. (Trautwine.)

lce and Snow. (From Clark.) 1 cubic foot of ice at 32° F., weighs 57.50 lbs.; 1 lb. of ice at 32° F., has a volume of .0174 cu. ft.=30.067 cu. in.

Relative volume of ice to water at 32° F., 1.0855, the expansion in passing into the solid state being 8.55 per cent. Specific gravity of ice=0.922, water at 62° F., being 1.

At high pressures the melting point of ice is lower than 32° F., being at the rate of .0133° F., for each additional atmosphere of pressure.

The specific heat of ice is .504, that of water being 1.

1 cubic foot of fresh snow, according to humidity of atmosphere: 5 lbs. to 12 lbs. 1 cubic foot of snow moistened and compacted by rain: 15 lbs. to 50 lbs. (Trautwine.)

Specific Heat of Water. (From Clark's Steam-engine.) Calculated by means of Regnault's formula, $c = 1 + 0.00004t + 0.000009t^2$, in which c is the specific heat of water at any temperature, t in centigrade degrees, the specific heat at the freezing point being 1.

Compressibility of Water. Water is very slightly compressible. Its compressibility is from .000040 to .000051 for one atmosphere, decreasing with increase of temperature. For each foot of pressure distilled water will be diminished in volume .0000015 to .0000013. Water is so incompressible that even at a depth of a mile, a cubic foot of water will weigh only about half a pound more than at the surface.

Water is composed of two gases, hydrogen and oxygen, in the ratio of two volumes of former to one of the latter. It is never found pure in nature, owing to the readiness with which it absorbs impurities from the air and soil.

One foot of water column at 39.1° F. = $62\ 425$ lbs. on the square foot.

One foot of water column at 39.1° F. = 0.4335 lbs. on the square inch.

One foot of water column at 39.1° F. = 0.0295 atmospheric pressure.

One foot of water column at 39.1° F. = 0.8826 in. mercury column at 32° F.

One foot of water column at 39.1° F. = 773.3 ft. of air column at 32° F. and atmospheric pressure.

One lb. pressure on sq. ft. = 0.01602 ft. water column at 39.1° F.

One lb. pressure on sq. in. = 2.307 ft. water column at 39.1° F.

One atmospheric pressure = 29.92 in mercury column = 33.9 ft. water column.

One inch of mercury column at 32° F.= 1.133 ft. water column.

One foot of air column at 32° F. and 1 atmospheric pressure = 0.001293 ft. water column.

WATER HAMMER

Extracts from Paper by O. Simin, Read Before the Twenty-fourth Annual Convention of the American Water Works Association.

The question of the so-called "water hammer" or "hydraulic shock" caused by stopping the flow in a water pipe, is of great practical importance, as the shock frequently bursts the pipe.

Geo. N. Peck describes water hammer as follows:

"When a liquid is flowing through a pipe there is a certain amount of energy in the liquid, and if we stop the flow this energy must be used up in some way.

"If the liquid is incompressible, and we stop the flow suddenly, the energy of the liquid is used up in doing work on the pipe by stretching it or increasing its diameter.

"If the liquid is compressible, the energy of the liquid is used up in compressing the liquid and stretching the pipe. Nearly all bursting of pipes is due to a sudden checking of the velocity of the liquid or to the freezing of the liquid."

The following summary and conclusions are based on exhaustive experiments conducted by Prof. Joukovsky, of Moscow, Russia, to determine the effects of water hammer in pipes.

1. The shock pressure is transmitted through the pipe with a constant velocity, which seems to be independent of the intensity of the shock. This velocity depends upon the elasticity of the material of the pipes and upon, the ratio of the thickness of their walls to their diameter.

Ordinarily, in cast-iron pipes the ratio of thickness to diameter decreases somewhat with increase of the diameter; hence the velocity of the pressure wave is a little less, in pipes of large diameters, than in pipes of smaller diameters.

For pipes of diameters from 2 to 6 inches this velocity is about 4,200 feet per second; for 24-inch pipe it is about 3,290 feet per second.

The speed of propagation of the pressure wave remains the same, whether the shock is caused by arresting the flow of a column of water moving in a pipe, or by suddenly changing the pressure in the column of water (flowing or standing) in any part and by any other means.

2. The shock pressure is transmitted along the pipe with constant intensity. The shock pressure is proportional to the destroyed velocity of flow and to the speed of propagation of the pressure wave. For ordinary cast-iron pipes, of diameters from two to six inches, the increase of pressure, for every foot per second of extinguished velocity of flow, is about four atmospheres (58.8 lbs.) and for a twenty-four inch pipe, about three atmospheres (44.1 lbs.)*

*For example: By suddenly closing a valve on a line, from two to six inches in diameter, in which the water is flowing at a velocity of five lineal feet per second, would cause an increase of pressure or "water hammer" of approximately 294 lbs., and this shock pressure would be transmitted along the entire length of the pipe with constant intensity.

Cubic Feet	Gallons	Cubic Feet	Gallons
$\begin{array}{c} 0.1\\ 0.2\\ 0.3\\ 0.4\\ 0.5\\ 0.6\\ 0.7\\ 0.8\\ 0.9\\ 1\\ 2\\ 3\\ 4\\ 5\\ 6\\ 7\\ 7\\ 8\\ 9\\ 10\\ 20\\ 30\\ 40\\ 50\\ 60\\ 70\\ 80\\ 90\\ 100\\ 200\\ 300\\ 400\\ 500\\ 60\\ 0\\ 200\\ 200\\ 300\\ 400\\ 500\\ 60\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0$	$\begin{array}{c} 0.75\\ 1.50\\ 2.24\\ 2.99\\ 3.74\\ 4.49\\ 5.24\\ 5.98\\ 6.73\\ 7.48\\ 14.9\\ 22.4\\ 29.9\\ 37.4\\ 44.9\\ 52.4\\ 59.8\\ 67.3\\ 74.8\\ 14.9\\ 52.4\\ 59.8\\ 67.3\\ 74.8\\ 14.9\\ 52.4\\ 59.8\\ 67.3\\ 74.8\\ 14.9\\ 528.4\\ 673.2\\ 748.0\\ 1,496.1\\ 2,244.1\\ 2,992.2\\ 3,740.2\\ 3,740.2\\ \end{array}$	$\begin{array}{c} 600\\ 700\\ 800\\ 900\\ 1,000\\ 900\\ 2,000\\ 3,000\\ 4,000\\ 5,000\\ 6,000\\ 9,000\\ 10,000\\ 20,000\\ 10,000\\ 20,000\\ 70,000\\ 80,000\\ 90,000\\ 100,000\\ 200,000\\ 100,000\\ 200,000\\ 1,000,000\\ 1,000,000\\ 1,000,000\\ \end{array}$	$\begin{array}{c} 4,488.3\\ 5,236.3\\ 5,984.4\\ 6,732.4\\ 7,480.0\\ 14,961.0\\ 22,441.5\\ 29,922.0\\ 37,402.6\\ 44,883.1\\ 52,363.6\\ 59,844.1\\ 67,324.6\\ 74,805.2\\ 149,610.4\\ 224,415.6\\ 299,220.7\\ 374,025.9\\ 448,831.4\\ 523,636.3\\ 598,441.5\\ 673,246.7\\ 748,051.9\\ 1,496,103.8\\ 598,441.5\\ 7374,025.9\\ 448,831.4\\ 523,636.3\\ 598,441.5\\ 7,2,992,207.6\\ 3,740,259.5\\ 448,831.4\\ 5,236,363.3\\ 5,984,415.2\\ 6,732,467.1\\ 7,480,519.0\\ \end{array}$

Showing U. S. Gallons in Given Number of Cubic Feet

From the above any cubic feet reading can readily be converted into U. S. gallons, as follows :

How many gallons are represented by 53,928 cubic feet?

50,000	cubic feet	=	374,025.9	gallons	
3,000			22,441.5	"	
900	"	=	6,732.4	66	
20			149.6	"	
8	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	=	59.8	44	
53,928	cubic foot	_	102 100 0	11	

928 cubic feet = 403,409.2 gallons

CISTERNS	and the second	11 12
KS AND	TLONS	10
ID TANH	* DEPTH IN FEET AND CONTENTS IN GALLONS	6
ROUN	CONTEN	00
ONS OF	FET ANI	2
GALLO	F NI HT	9
NTS IN	* DE	20
ONTE	1.000 C	4
VING 0		ľ.
TABLE SHOWING CONTENTS IN GALLONS OF ROUND TANKS AND CISTERNS	Diameter in	Feet

 * To ascertain contents of a round tank or cistern of the above diameters, and of depth not given, multiply the contents of tank one foot deep by the required depth in feet.

1128. 1763. 25538. 3455. 4512. 5711. 7050. 8531.

1034. 1616. 2327. 2327. 3167. 53235. 5462. 7819.

940. 1469. 2115. 2115. 2879. 3760. 4759. 5875. 7109.

846. 1322. 1914. 2591. 3384, 4283. 5288. 6398. 7614.

752. 1175. 1692. 2308. 3008. 3806. 3806. 5687. 6768.

658. 1028. 1481. 2015. 2632. 3331. 4113. 5922.

564. 881. 1269. 1727. 2256. 2855. 3525. 3525. 5076.

470.734.1058.1439.1439.2379.2554.3554.

376. 588. 5847. 1152. 1504. 1504. 1904. 2350. 3384.

93.99 146.87 211.50 287.86 375.98 375.98 475.85 587.47 710.84 845.97

410000000000000

TABLE SHOWING CONTENTS IN GALLONS OF SQUARE TANKS AND CISTERNS

140.5	1 8.	Gallens in General
isolasi Totasi	12	1436. 2244. 3231. 4398. 5745. 8976. 8976. 10861. 12925.
	11	1316. 2057. 2968. 4032. 5266. 88228. 9956. 11848.
TLONS	10	1197. 1870. 2693. 2693. 3665. 4787. 6059. 6059. 7480. 9051. 10771.
TS IN GA	6	1077. 1683. 2424. 3299. 4308. 5453. 6732. 8146. 8146.
CONTENTS IN GALLONS	00	957. 1516. 2154. 2922. 3830. 4847. 5984. 7241. 8617.
ET AND	2	838. 838. 1309. 1385. 2566. 3351. 4241. 5236. 6336. 6336. 7540.
DEPTH IN FEET	9	718. 1202. 1616. 2199. 2872. 2872. 2872. 2872. 2872. 5430. 6463.
* DEPI	5	598. 935. 935. 1346. 1333. 1333. 2394. 2394. 2329. 3740. 5386.
and a local	4	$\begin{array}{c} 479.\\ 748.\\ 1077.\\ 1915.\\ 2424.\\ 2992.\\ 3620.\\ 4308. \end{array}$
ant a	I*	$\begin{array}{c} 119.68\\ 187.00\\ 269.28\\ 366.52\\ 478.72\\ 605.88\\ 748.00\\ 905.08\\ 905.08\\ 1077.12\end{array}$
Dimensions of	Bottom in feet	4 x 4 5 x 5 7 x 7 7 x 7 8 x 8 8 x 8 9 x 10 10 x 10 11 x 11 12 x 12

 * To ascertain the contents of a square tank or cistern of depth not given, multiply the contents of tank one foot deep as in table by the required depth in feet.

TABLE SHOWING EQUIVALENTS OF PRESSURE AND HEAD OF WATER

TN	KOO T ha	Feet Hood	415.6 445.6 438.9 461.7 519.5 577.2 643.0 692.7 750.4 808.1 922.7 750.4 808.1 922.7 750.4 1154.5
EQUIVALENT	1 120 40 5		225 225 225 225 225 225 225 225 225 225
AND	N L'bs		161.6 184.7 2073.9 253.9 253.9 253.9 253.9 253.9 253.9 255.9 255.9 255.9 255.9 255.9 255.9 255.9 255.9 255.9 255.9 257.0
N POUNDS HEAD IN	70 to 170	Lbs. Press	70 100 110 110 110 110 110 110 110 110 1
PRESSURE IN POUNDS HEAD IN	Lbs.	Feet	11.5 23.0 23.0 23.0 246.2 57.7 69.3 80.8 80.8 80.8 80.8 80.8 80.8 115.4 115.4 115.4 115.4 115.4
PRE	5 to 60	Libs. Press	110 110 110 110 110 110 110 110 110 110
SURE	000 feet	Lbs. Press	86,6 108,2 151,5 151,5 151,5 173,2 216,5 259,8 303,1 336,4 3389,7 433,0
NT PRESSURE	,200 to 1,000 feet	Feet Head	200 250 300 350 400 500 500 500 500 500 500 500 500 5
HEAD IN FEET AND EQUIVALENT IN POUNDS 5 to 60 feet 70 to 180 feet 200	30 feet	Lbs. Press	20.3 34.6 334.6 334.6 334.6 47.6 55.3 56.3 56.3 56.3 60.6 60.6 60.6 60.6 57.0 78.0
	70 to 18	Feet Head	70 80 80 1100 1100 1100 1120 1120 1150 1150 1160 1180
	0 feet	Lbs. Press	$\begin{array}{c} 2.17\\ 2.17\\ 4.33\\ 6.50\\ 8.66\\ 10.88\\ 15,16\\ 15,16\\ 17,32\\ 15,16\\ 17,32\\ 21.65\\ 22.09\\ $
	5 to 6	Feet Head	600544053325051110 m 6005440533250505110 m 6005440533250505110 m

13

Loss by Friction of Water in Pipes— Continued

per ite.	SI	ZES C)F PI	PE-	-INS	IDE D	IAME	TER.
Gals. per minute.	4 in.	6 in.	8 in.	10 in.	12 in.	14 in.	16 in.	18 in.
5 100 155 200 255 300 2550 150 1755 2000 2500 3000 3500 4500 5000 4000 4500 5000 5000 5000 12550 12500 1275000 1275000 1275000 1275000000000000000000000000000000000000	in. in. in. in. in. in. in. in.	in. 	in. 	in. 	in. 	in. 	in. 	in.
2000 2250 2500 3000 3500 4000 4500	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·				$\begin{array}{c} 0.515 \\ 0.697 \\ 0.910 \end{array}$	$\begin{array}{c}\\ 0.188\\ 0.267\\ 0.365\\ 0.472 \end{array}$	$0.150 \\ 0.204 \\ 0.263$
5000]				0.593 0,730	

USEFUL FACTORS FOR WATER

Based on Weights at 62° F. (Standard Temperature)

U.S. Gallons x $8.3356 = pounds$
x 231 — authia in at an
X 83356 - English and I
X 3.78544 - Litons
\therefore \therefore \therefore $2020985 = Kokus, Japan$
x .30815 = Bedeps Russia
English C-11
$\begin{array}{ccc} & x & .160372 = \text{cubic feet} \\ & x & 277.12 & = \text{cubic inches} \end{array}$
x 45413 = Titong
X 025175 = Kokurg Tomor
x .36969 = Bedeps. Russia
T 11.
x 61 023 = aubic in above
* x $26417 = II S$ collors
" $x_{2202} = English gallong$
x .0055435 = Kokus, Japan
x .081405 = Bedeps, Russia
TZ 1
$\begin{array}{c} x \ 11008.00 = \text{cubic inches} \\ x \ 47.6535 = U. S. \text{ gallons} \end{array}$
X = 39 / 22 / 128 = Finaliah = 11
X 18U 39 = Litors
" $x = 14,6847 = Bedeps, Russia$
D.1. OF SE
" x 749 618 oubic in share
" $x 3.24512 = U S$ collors
x 2.705 = Engligh collows
" x $12.2843 = \text{Litorg}$
" x $.0680983 = $ Kokus, Japan
C.1: C
x 28 217 - Literra
15609 - Kolmer T
$\begin{array}{cccc} & & & & & \\ & & & & \\ & & & & \\ & & & \\ & & & & & \\ & & & & \\ & & & & \\ & & & & & \\ & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & $
Describer de la construction de
$\begin{array}{cccc} & & & \\ & & & & \\ & & & \\ & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & $
v 45419 - Litowa
x = 0025175 = Kokana Toman
" " x .036969 = Bedeps, Russia
Deuchs, Russia

STEAM.

A cubic inch of water, evaporated under ordinary atmospheric pressure, will be converted into, approximately, one cubic foot of steam, and it exerts a mechanical force equal to lifting 2,120 pounds one foot high.

27,222 cubic feet of steam weighs one pound.

13.817 cubic feet of air weighs one pound; the specific gravity of steam, atmospheric pressure, being 411 that of air at 34°F., and .0006 that of water at the same temperature.

Each nominal horse-power of boilers requires from four to eight gallons of water per hour.

In calculating the horse-power of boilers allow for tabular boilers 15 square feet, for flue boilers 12 square feet, and for cylinder boilers 10 square feet of heating surface per horse-power.

The unit of power for boilers adopted by the Committee of Judges of the Centennial Exhibition is as follows: One horse-power equals 30 pounds of water evaporated into dry steam per hour from feed water at 100°F., and under a pressure of 70 lbs, per square inch above the atmosphere.

One square foot of grate surface will consume from 10 to 12 pounds of hard coal, or from 18 to 20 pounds of soft coal, per hour, natural draft. With forced draft these amounts can be doubled.

Good boilers will evaporate from 7 to 10 pounds of water per hour per pound of coal.

Steam at a given temperature is said to be saturated when it is of maximum density for that temperature. Steam in contact with water is saturated steam.

Steam which has water (in the form of small drops) suspended in it is called wet or supersaturated steam. If wet steam be heated until all the water suspended in it is evaporated, it is said to be dryed.

If dry saturated steam be heated when not in contact with water, its temperature is raised and its density is diminished or its pressure is raised. The steam is then said to be super-heated.

Let W=weight of a given quantity of wet steam, w=weight of water suspended in this steam, then dryness fraction=W-w

W

Under ordinary conditions and good stoking the dryness fraction is about 95 per cent.

Circumference and Areas of Circles

D=Diameter of Circle A=Area of Circle

 $A = \frac{1}{4} D^{2} = .785398 D^{2}$ $D = \frac{2}{\sqrt{A}} = 1.128379 \sqrt{A}$

	and the second se		4.		and the second second
Diam.	Circum.	Area.	Diam.	Circum.	Area.
10430230476 1944948848 4424 14294 142	$\begin{array}{c} .39270\\ .78540\\ 1.1781\\ 1.5708\\ 1.9635\\ 2.3562\\ 2.7489\\ 3.543\\ 3.9271\\ 4.3197\\ 4.7124\\ 5.1051\\ 5.4978\\ 5.8905\\ 6.2832\\ 7.0686\\ 7.8540\\ 8.6394\\ 9.4248\\ 10.210\\ 10.996\\ 8.6394\\ 9.4248\\ 10.210\\ 10.996\\ 1.3552\\ 14.137\\ 14.923\\ 15.708\\ 16.493\\ 17.279\\ 18.064\\ 18.850\\ 19.635\\ 20.420\\ 19.635\\ 20.420\\ 21.991\\ 22.776\\ 23.562\\ 24.347\\ 25.133\\ 25.918\\ 25.133\\ 25.918\\ 25.7489\\ \end{array}$		$\begin{array}{c} 9\\ 9\\ 9\\ 9\\ 9\\ 9\\ 9\\ 9\\ 9\\ 9\\ 9\\ 9\\ 9\\ $	$\begin{array}{c} 28.274\\ 29.060\\ 29.845\\ 30.631\\ 31.416\\ 32.201\\ 32.987\\ 33.752\\ 34.558\\ 35.343\\ 36.128\\ 36.128\\ 36.914\\ 37.699\\ 38.485\\ 39.270\\ 40.055\\ 40.841\\ 40.055\\ 40.841\\ 41.626\\ 42.412\\ 43.197\\ 43.982\\ 44.768\\ 42.412\\ 43.197\\ 43.982\\ 44.768\\ 45.553\\ 46.338\\ 46.338\\ 47.124\\ 43.982\\ 44.768\\ 45.553\\ 51.836\\ 65.549\\ 51.836\\ 65.549\\ 55.549\\$	$\begin{array}{c} 63.617\\ 67.201\\ 70.88\\ 74.66\\ 78.54\\ 82.52\\ 86.59\\ 99.0.76\\ 95.03\\ 99.40\\ 103.87\\ 108.43\\ 113.10\\ 103.87\\ 108.43\\ 113.10\\ 117.86\\ 122.72\\ 127.68\\ 132.73\\ 137.89\\ 143.13\\ 143.49\\ 153.94\\ 153.94\\ 153.94\\ 153.94\\ 153.48\\ 165.13\\ 170.87\\ 176.71\\ 182.65\\ 138.69\\ 194.83\\ 201.06\\ 213.82\\ 226.98\\ 240.53\\ 213.82\\ 226.98\\ 240.47\\ 268.80\\ 228.53\\ 298.65\\ 314.16\\ 330.06\\ 346.36\\ 380.13\\ 397.61\\ 415.48\\ \end{array}$
)	And a state of the state of the	1	and the second product of	

Circumferences and Areas of Circles

(CONTINUED.)

Diam.	Circum.	Area.	Diam.	Circum.	Area.
231%	-				-
24	73.827	$433.74 \\ 452.39$	$ 47 \\ 47 \frac{1}{2} $	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1734.9 1772.1
$24\frac{1}{2}$ 25	76.969 78.540	471.44 490.87	48 481/2	150.796 152.367	1809.6 1847.5
251/2	80.111	510.71	49	153.938	1885,7
$\frac{26}{26\frac{1}{2}}$	81.681 83.252	530.93	491/2	155.509	1924.4
2072	84.823	551.55 572.56	50 50 1/2	157.080 158.650	1963.5 2003.0
271/2	86.394	593.96	51	160.221	2003.0
28	87.965	615.75	511/2	161.792	2083.1
28%	89.535 91,106	$637.94 \\ 660.52$	$52 \\ 52 \frac{1}{2}$	$163.363 \\ 164.934$	2123.7
291/2	92.677	683.49	53	164.934	2164.8 2206.2
30	94.248	706,86	531/2	168.075	2248.0
$30\frac{1}{2}$ 31	95.819 97.389	730.62	54	169.646	2290.2
31%	98,960	754.77 779.31	541/2	171.217	2332.8 2375.8
32	100.531	804.25	551/2	174.358	2419.2
321/2	102.102	829.58	56	175.929	2463.0
$\frac{33}{33\frac{1}{2}}$	103.673 105.243	855.30 881.41	$56\frac{1}{2}$ 57	177.500	2507.2
34	106.814	907.92	571/2	179.071 180.642	2551.8 2596.7
341/2	108.385	934.82	58	182.212	2642.1
$35 \\ 35\frac{1}{2}$	109.956	962.11	581/2	183,783	2687.8
36	111.527 113.097	989.80 1017.9	59 59½	185,354 186,925	2734.0 2780.5
361/2	114.668	1046.3	60	188.496	2180.5
37	116.239	1075.2	601/2	190,066	2874.8
371/2	117.810 119.381	1104.5 1134.1	61	191.637	2922.5
381/2	120.951	1134.1 1164.2	$61\frac{1}{2}$ 62	$193.208 \\ 194.779$	$2970.6 \\ 3019.1$
39	122.522	1194.6	621/2	194.779	3068.0
391/2	124.093	1225.4	63	197.920	- 3117.2
40 40 ¹ / ₂	$125.664 \\ 127.235$	1256,6 1288.2	631/2	199.491	3166.9
41	128.805	1320.3	$64 \\ 64^{1/2}$	201.062 202.633	$3217.0 \\ 3267.5$
411/2	130,376	1352.7	65	204.204	3318.3
42 42 ¹ / ₂	131.947	1385.4	$65\frac{1}{2}$	205.774	3369.6
42½ 43	$133.518 \\ 135.088$	1418,6 1452,2	66	207,345	3421.2
431/2	136.659	1452,2		208.916 210.487	3473.2 3525.7
44	138.230	1520.5	671/2	212,058	3578.5
441/2	139.801	1555.3	68	213.628	3631.7
45 45½	$141.372 \\ 142.942$	1590.4 1626.0		215.199	3685,3
46	144.513	1661,9	$69^{1}/_{2}$	216,770 218.341	3739.3 3793.7
461/2	146.084	1698,2	70	219.911	3848,5
	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Contract 1	Surray and	- 1 - acre - 1	AL 8.0

WEIGHTS AND MEASURES

Troy Weight

24 grains=1 pwt. 12 ounces=1 pound. 20 pwts.=1 ounce.

Used for weighing gold, silver and jewels.

Apothecaries' Weight

20 grains=1 scruple. 3 scruples=1 dram. 8 drams=1 ounce. 12 ounces=1 pound. The ounce and pound in this are the same as in Troy weight.

Avoirdupois Weight

27 11-32 grains=1 dram.	4 qu
16 drams=1 ounce.	2,000
16 ounces=1 pound.	2,240
25 pounds=1 quarter.	

arters=1 cwt. 0 lbs.=1 short ton. 0 lbs.=1 long ton.

Dry Measure

2 pints=1 quart. 8 quarts=1 peck.

4 pecks=1 bushel. 36 bushels=1 chaldron.

Liquid Measure

gins=1 pint. pints=1 quart. quarts=1 gallon.	31½ gallons=1 barrel. 2 barrels=1 hogshead.
--	--

Time Measure

60 seconds=1 minute. 24 hours=1 day. 60 minutes=1 hour. 7 days=1 week. 28, 29, 30 or 31 days=1 calendar month (30 days=1 month in computing interest). 365 days=1 year.

366=1 leap year.

Circular Measure

60 seconds=1 minute. 30 degrees=1 sign. 60 minutes=1 degree. 90 degrees=1 quadrant. 4 quadrants=12 signs, or 360 degrees=1 circle,

Long Measure

12 inches=1 foot. 3 feet=1 yard. 51/2 vards=1 rod.

40 rods=1 furlong. 8 furlongs=1 sta. mile. 3 miles=1 league.

4 quarters=1 yard.

Cloth Measure

2¼ inches=1 nail. 4 nails=1 quarter.

Mariners' Measure

6 feet=1 fathom. 120 fath.=1 cab. length. 5,280 feet=1 sta. mile. 6.085 feet=1 naut. mile. 7½ cable lengths=1 mile.

Miscellaneous

3 inches=1 palm. 4 inches=1 hand. 6 inches=1 span.

18 inches=1 cubit. 21.8 in.=1 Bible Cubit. 2½ ft.=1 Military pace.

Square Measure

144 sq, in.=1 sq. foot. 9 sq. feet=1 sq. yard. 3014 sq. yards=1 sq. rod. 640 acres=1 sq. mile.

40 sq. rods=1 rood. 4 roods=1 acre.

18

Surveyors' Measure

7.92 inches=1 link. 4 rods=1 chain. 25 links=1 rod. 10 sq. chains or 160 square rods=1 acre. 640 acres=1 sq. mile. 36 sq. miles (6 miles sq.)=1 township.

Cubic Measure

1,728 cubic in.=1 cu, ft. 128 cu, ft.=1 cord (wood) 27 cubic ft.=1 cu. yd. 40 cu.ft.=1 ton(shpg.) 2,150.42 cu, inches=1 standard bushel. 268.8 cu, inches=1 standard gallon. 1 cu. foot=about four-fifths of a bushel.

Metric Equivalents

Linear Measure

1 centimeter=0.3937 in. 1 decimeter=3.937 in.= 0.328 feet. 1 meter=39.37 in.= 1.0936 vards. 1 dekameter=1 9884 rods. 1 kilometer=0.62137 mile.

- 1 in.=2.54 centimeters. 1 ft =3.048 decimeters 1 yd.=0.9144 meter. 1 rod=0.5029 dekameter.
 - 1 mile=1,6093 kilometers
- Square Measure 1 sq. in.=6.452 square
- 1 sq. centimeter=0.1550 sq. in. 1 sq. decimeter=0.1076
- sq. feet.
- 1 sq. meter=1.196 sq. yds.
- 1 are.=3.954 sq. rods.
- 1 hektar=2.47 acres.
- 1 sq. kilometer=0.386 sa.m.
- 1 sq. foot=9.2903 square decimeters. sq. yd.=0.8361 square
- meter. 1 sq. rod=0.2529 are.

centimeters

1 sq. mile=2.59 square

Measure of Volume

- 1 cu. centimeter=0.061 cu. in. 1 cu. decimeter=0.0353) cu. ft. $\frac{1 \text{ cu. meter}}{1 \text{ ster}} = \begin{cases} 1.308 \text{ c. yd. } 1 \text{ cu. yd.} = 0.7646 \text{ cu. met.} \\ 0.2759 \text{ cd. } 1 \text{ cord} = 3.624 \text{ sters.} \end{cases}$ (0.908 gt. dry 1 liter= { 1.0567 qts. liq. 1 dekaliter= $\left\{ \frac{2.6417}{2.6417} \text{ gals.} \right\}$.135 peck. 1 heckto .= 2.8375 bushels.
 - Weights
- 1 gram=0.0527 ounce. 1 kilogram=2.2046 lbs. 1 metric ton=1,1023 Eng-) lish tons
- 1 ounce=28.35 grams. 11b.=0.4536 kilogram. 1 English ton=0.9072

Approximate Metric Equivalents

- 1 decimeter=4 inches. 1 meter=1.1 yards. 1 kilometer $= \frac{5}{8}$ of mile. 1 hektar $= \frac{21}{2}$ acres. 1 ster. or cu. meter=1/4 of) a cord.
- 1 liter= $\begin{cases} 1.06 \text{ qts. liquid.} \\ 0.9 \text{ qt. dry.} \end{cases}$ 1 hektoliter=2% bu 1 kilogram=21-5 lbs. 1 metric ton=2,200 lbs.

ADDRESSES

- 1 acre=0.4047 hektar. kilometers. 1 cu. in.=16,39 cu. centimeters. 1 cu, foot=28.317 cu, deci-
- meters.
- 1 qt. dry=1.101 liters.
- 1 qt. liq .== 0.9463 liters.
- 1 gal.=0.3785 dekaliter.
- 1 peck=0.881 dekaliter. 1 bu.=0.3524 hektoliter.

metric ton.

MEMORANDA ADDRESSES miss Lilian Sillette Cook 165 West 82nd St. new york. also- Long Lea Farm anheret. mass James Mills, Supt. arlington Heighte Riverside, Calif. Clara Barrus 130 West 104 th St. New york. C/o Dr. Johnson.

MEMORANDA MEMORANDA This gaelet, 647 with an mrs. a. H. Sellers were year youk 320 Weit Californialt Pasadena, Cal. Jar Wyllie (Denisor) mrs. Dickey 407 Clcott Place Pasadena, Cal. Alort Road Cape Town. mrs. J. n. Russell S. Africa 2263 Hobart Blod Los angeles, Charles Reeler 2727 Diviglet Way Bertagley my Ayers St. Georges St. Jours N. S. Tinnina Mr. Kilharing Harthare martinez . 3255 Paufic ann. 5. J. Cal HER Calif. mon Buch A, Frank 110 Minthe St. 233 Formosa and Pacific Grove, Hollowood Cal

MEMORANDA MEMORANDA Mrs. Morris Thompson, 3100 North Griffin ave. Los Angeles, Calif. . Mrs. Fred Hooker Jones 325 West adams St. Los Angeles Paly

Notes from Mary Kingsley & Wart MEMORANDA Readdocen Vanc of Maprica Landolphia florida (Ovar mituris > landamus candelabrum with for itely demps, two. + " foran chair explorements "1 Lamblike calf header nead " Suburban agnostics " On all sides riges the colossal liona having bourst merward with the glking en The riverse Thereach reason & alking - In the Come and the energy lightning comes down into florigets m greep forthe plashes + approling around & reugh Thomas It clarming as many ficting · herblockword of seven ; The heaving provoring suffer -- oating heat, + wident approchemences of all living things, when the planner b buriets & roan if hanne Repart at live manage of the

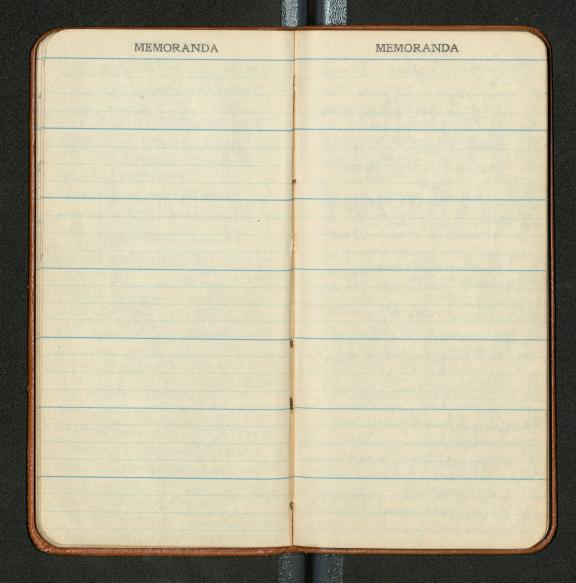
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nother MEMORANDA MEMORANDA There bearing of boling The same grups comp Mungo Walk. Solak, - The Showing Pistia stratistis, makes of "Immiden" The great gloating islands some Mak of Cameroon Slowly sworling round recent 13760 for high many m Eding and denly night up out They great nothern of Vinn of The agen in hule close af Allante meeting here man have to platigard towers Jorah charthe anna Varg The lovely adams mass of Tophe Coope Horan -Filmando Po to 10,190 At Natures say of your gave The Every time, your pars it by grass too soon or when The becauted around on you There is no wind you tall with cheater greater at antonight i But of Jun weit gavere. The up to arever twice until it is very drig you drift The advance. Segue fromes wies attain Kill it, Because Mar Stran with and so black cloger grows in tufts from bull ametimes softly gorgaous with gold, green, + hugen I the first gammed by the entired rapors tinded by it swalps hapilly to bese ty the setting since No without heating the roots instead of smonthly a boundaries cristed with snow long enough to the them constants conjectedly swath your bank see that all The happy corkensaring best when you once know of stay at home subwalled agnostics regarding had you been down & worship 11 the Unaverses

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MEMORANDA MEMORANDA led no to bes trus! These of conscientions " All disagreeables A sight to gladding any ben fele ane guardian angel in the lay, (an Eliphant varippom weitertching a grante in desthe Those with queen The armed Thabe that his Ibeardenly Fathars Nahers " protection assumed. He belenver in hunnelf Notes prom Oundas Heliam thing Deite as the creator t Septender of himself. The Kindness of Mahare is generally This and it The ansara impulse of the sportegen an to by the ingenety + devilous Shill every thing or man. Hunters who Would cat any abnowit abre hunging there of Dirk in the services hunging childrens at home a any burg prouded and typenger , but not We sigh was the washing the sheer pleasant of a gold par of of second the agomes Ras has non injoyed life & have not all the good physicians

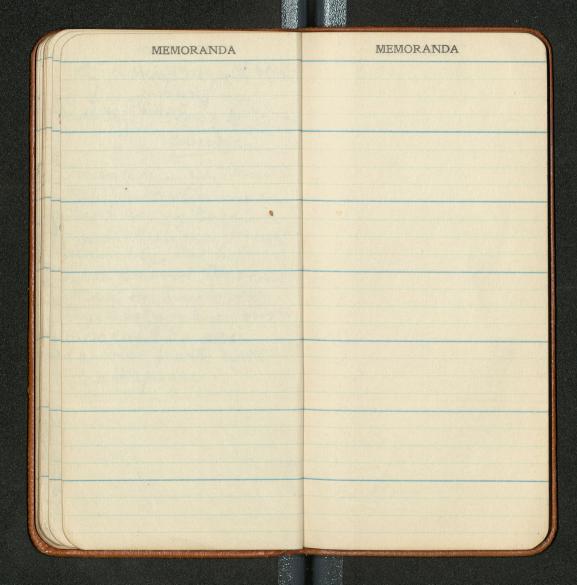
Note MEMORANDA Syon. MEMORANDA aber provins a Jestiral Fightime, the slave For they unhappy mining tintensin Central the children of 0, for Africa" By the Striving ; for the seeker of inardinate en-Joymuth, for the A fred J. Swann -Fran equition on thusiasi ambitions for the sense Solitude is but ill-- strange closery of shares adapted ". m that tabat wilder of that enobling the "So long" sailorsphra heart & strangthings of for holy nesstrations agaran " From Kupert of Hem - zan A. Hope) The rains were now aver (Jun or July) but Jernes chamge for all i youth gois 22 Frehl 5 for the way not burne Ostream offile Onks up by this derastating a quit glow " fires who annually In the agest ailing the severp over nearly hope of the breed all tropersal aprica destroying or strending most of the young trees

MEMORANDA MEMORANDA you know you can't It is This repeated sconching, Why partly accounts for the wet ful youte is the Thunder apecimento or Trees ghowing in most That Kills, you are ashint & april making charcoat deserts not the loghtnesse To & Jude your clums. on the Blantyre Soft That fear in this holes. Gamber manut + toke tower the after The brokasphere of Sumaptions. nabour does not the shupping ander Gitte your morade. a gigantre baobas tru a Joure White Propo Strange on A mare appear I pever t nearks Mary Mollat Grance. Mrs Lowellow heard of home allacking any of those diseased percons isileter writches 11 lift antide the Neldong wall: taushed Boys leaving the in a rowing live a kape and ak Jungan disbarning any attemp af defence - challing The breat to do its worst know more about "Come This way + Jenshing porredges

MEMORANDA MEMORANDA Throah Than purshing by Hall Carn My story a canve " get and + carry the boat Thredling acuse of the you will go a rastruces it Os the mighting Cecil Phody what I helt 50 yrs ago thought in Continuity about the sale of Man - Thesto it was the whyle O un little, that all the catercelle, all the passions They astrend Why Dorgon. Keep on prayment your bor? Is he alizanjo + allow all the experience that logk in the nish watching for an de-- partisally to infine See - has been the motion enstroning my pooks of preventing bed spining parthing medgerments Sore of I have twened anothing by 5+20 Mps of almast continuous Our spirits ner is one the serve everywhile slads & we let them. alon as much as poss + that nothing I had tengen spla . V our time many race has out of thermony will great & maall at the

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SOUTH CHESTER GENUINE WROUGHT IRON CASING

Inside	W	ani -
Diameter,	Weight	Threads
	Per Foot,	Per
Inches	Pounds	Inch
41/4	6.36	
41/4		14
41/2	6.73	14
41/2		14
5 3-16		1116
5%		14
5%	14,20	1116
5%		111
61		111
65%		10
7 5%		111
75%		
81/		
85%		
95%		
95/		
10		
105%		······ ð
115/		
1916		
131.	42.02	
1414		
154		
10-2		

SOUTH CHESTER CALIFORNIA WROUGHT IRON CASING

All 10 Thread

Inside	Outside	Weight
Diameter,	Diameter,	Per Foot
Inches	Inches	Pounds
5%	6	
61/	65%	90
61	65%	26
614	65%	98
65%		
65/		
0/8	······ / ,······	26
0/8		
1/8		· ····
81/4		
81/4		
81/4	85%	
81/4	85%	38
81/1	85%	.,00
9%	10	
10		40
10		45
10		18
10		54
11 %		
1212		
121/2		
121/2		
134/2		

MERCHANT PIPE.

Inside	Weight	
Diameter	Per Foot	Thread
Inches		Per
	Pounds	Inch
1/8		
	56	
3/4	1.12	
1	1.67	
1/4	····· Z.Z4	1
1 72		
		1114
472	5.74	8
	7.54	8
31/2		
4	10 00	
41/2	19 40	
5		The second second second
6	10 80	
8		0
9		
10		
12		8
		ð

LINE PIPE.

Inside	Weight	Test	Threads
Diameter	Per Ft.	Pounds	Per
Inches	Pounds	- oundb	
2	3.61		Inch
		1200	11142
07	3.61		
	5,74		8 & 11%
	7.54		
31/2			8 & 111/2
4			8 & 111/2
	10.10		8 & 10 .
		1500	8
6			8
7		1500	
		1200	
8	25.00	750	
8			8
9			8
10		1200	8
10	115 00	800	8
10	35.00		8
12	45.00	800	8
12			
			8

SOUTH CHESTER WROUGHT IRON TUBING.

Inside	Woinht	
Diameter	Weight	Threads
Inches	Per Foot	Per
11/4	Pounds	Inch
	2.24	
	4.00	
		· ····
21/2		······
	0.00	111/2
3		
3	8 50	
3		
31/2		
4		
4		8
41/2		8
6		
PT	18,76,	
8		

9		
10		
12	40.00	
		8

DRIVE PIPE. SOUTH CHESTER WROUGHT IRON

41/2-inch......15 Pound...... ...10 Thread

The second second	
Alaciona Di	All 8 Thread
Inside Diameter	Weight
Inches	Per Foot
21/2	Pounds
	5.74
	7.54
4	
41/2	

0	
7	
0	
10	33.70
19	

WHITLOCK Manila Drilling Cables

combine all that is essential in a first-class manila rope, selected long fibre carefully laid, and **besides** are lubricated in a way that keeps the cable flexible despite the drying character of California climate. A special non-drying lubricant does this. The practical value of this feature of Whitlock Cable is attested by **every** user.

We solicit inquiries and stand ready to demonstrate our claims.

000000000000000000000000000000000000000	000000000000000000000000000000000000000
8 1912 CALE	NDAR 1912
JANUARY	JULY
	S M T W T F S
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X 11 12 13 14 15 16 17 18 19 20 21 22 23 24	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
MARCH	25 26 27 28 29 30 31 SEPTEMBER
8 3 4 5 6 7 8 9	
X 10 11 12 13 14 15 16 17 18 19 20 21 22 23	8 9 10 11 12 13 14 15 16 17 18 19 20 21
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X 14 15 16 17 18 19 20 21 22 23 24 25 26 27	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
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$X \stackrel{\dots}{_5} \stackrel{\dots}{_6} \stackrel{\Pi}{_7} \stackrel{1}{_8} \stackrel{2}{_9} \stackrel{3}{_{10}} \stackrel{4}{_{11}}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
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	ch & Co., Phila.

